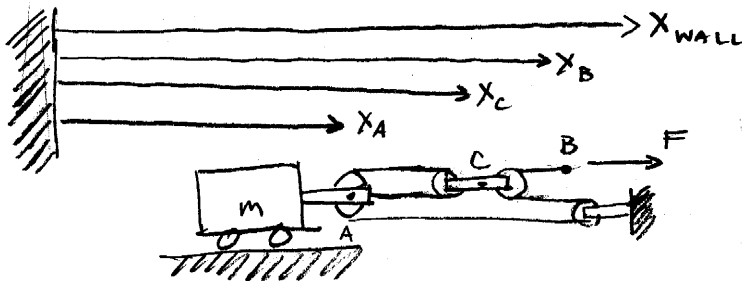


#12.19



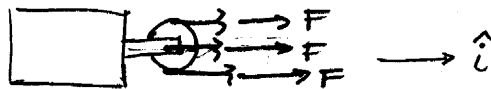
$L = \text{length of rope}$

$$\approx (x_{\text{wall}} - x_A) + 2(x_C - x_A) + (x_{\text{wall}} - x_C) + (x_B - x_C)$$

$$\Rightarrow -3\ddot{x}_A + \ddot{x}_B = 0 \quad \Rightarrow \quad \boxed{\ddot{x}_B = 3\ddot{x}_A} \quad (1)$$

Assuming massless pulleys the tension in the rope will be equal to the applied force F .

FBD of mass A



LMB for mass A

$$F = ma$$

$$3F \hat{i} = m \ddot{x}_A \hat{i}$$

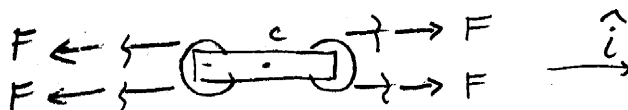
$$\Sigma \cdot \hat{i}$$

$$\Rightarrow \boxed{\ddot{x}_A = 3 \frac{F}{m}}$$

$$\textcircled{1}$$

$$\Rightarrow \boxed{\ddot{x}_B = 9 \frac{F}{m}}$$

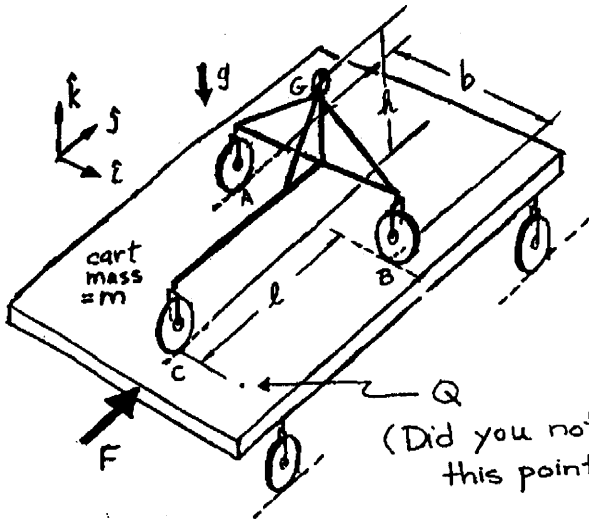
Finally, $\boxed{\ddot{x}_C = 0}$ from the following FBD & LMB



1)(30 pts) 3-wheeled robot. A 3-wheeled robot with mass m is being transported on a level flatbed trailer also with mass m . The trailer is being pushed with a force $F\hat{j}$. The ideal massless trailer wheels roll without slip. The ideal massless robot wheels also roll without slip. The robot steering mechanism has turned the wheels so that wheels at A and C are free to roll in the \hat{j} direction and the wheel at B is free to roll in the \hat{i} direction. The center of mass of the robot at G is h above the trailer bed and symmetrically above the axle connecting wheels A and B. The wheels A and B are a distance b apart. The length of the robot is ℓ .

Find the force vector \underline{F}_A of the trailer on the robot at A in terms of some or all of $m, g, \ell, F, b, h, \hat{i}, \hat{j}$, and \hat{k} .

[Hints: Use a free body diagram of the cart with robot to find their acceleration. With reference to a free body diagram of the robot, use angular momentum balance about axis BC to find F_{Ax} .]



Note: From the announcement,

$$\underline{a}_G = \underline{a}_{\text{CART}} = \underline{a}$$

The robot does not move with respect to the cart.

(Did you notice this point?)

$$m_{\text{ROBOT}} + m_{\text{CART}} = 2m$$

FBD (cart w/robot)

$$\text{LMB} : \Sigma \underline{F} = m_{\text{TOTAL}} \underline{a}$$

$$\text{LMB} \cdot \hat{j} \Rightarrow F = 2m a_y$$

$$\therefore a_y = \frac{F}{2m}$$

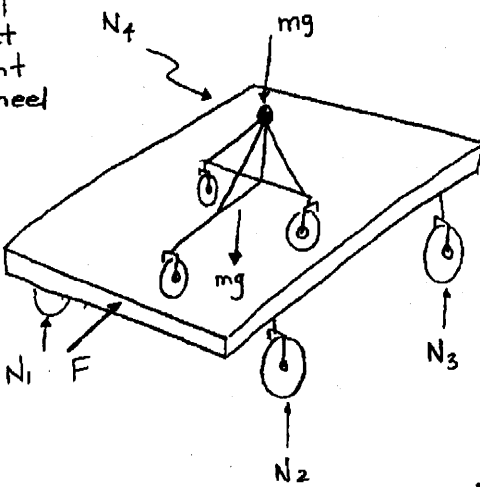
$$\text{LMB} \cdot \hat{i} \Rightarrow 0 = 2m a_x$$

$$\therefore a_x = 0$$

$a_z = 0$ by the assumption that the cart doesn't leave the ground

$$\therefore \underline{a} = \frac{F}{2m} \hat{j}$$

(Normal force at the front left wheel of the cart)



$$\underline{\Delta MB}/_{\text{axis BC}} : \{ \underline{\Sigma M}/_c = \dot{H}/_c \} \cdot \hat{\lambda}_{BC}$$

$$\text{where } \hat{\lambda}_{BC} = \frac{\underline{r}_{BC}}{|\underline{r}_{BC}|}$$

$$\Rightarrow \hat{\lambda}_{BC} = \frac{\frac{b}{2} \hat{i} + l \hat{j}}{\sqrt{(\frac{b}{2})^2 + l^2}}$$

The only forces creating moments about axis BC are A_z , mg :

$$\begin{aligned} \{ \underline{\Sigma M}/_c \} \cdot \hat{\lambda}_{BC} &= \{ \underline{r}_{A/c} \times A_z \hat{k} \\ &\quad + \underline{r}_{G/c} \times -mg \hat{k} \} \cdot \hat{\lambda}_{BC} \\ &= \{ (-\frac{b}{2} \hat{i} + l \hat{j}) \times A_z \hat{k} + (l \hat{j} + h \hat{k}) \times -mg \hat{k} \} \cdot \hat{\lambda}_{BC} \\ &= \{ +A_z \frac{b}{2} \hat{j} + A_z l \hat{i} - mgl \hat{i} \} \cdot \frac{\frac{b}{2} \hat{i} + l \hat{j}}{\sqrt{(\frac{b}{2})^2 + l^2}} \end{aligned}$$

$$= \left(\frac{b}{2} l (A_z - mg) + \frac{bl}{2} A_z \right) \frac{1}{\sqrt{(\frac{b}{2})^2 + l^2}}$$

$$\begin{aligned} \{ \dot{H}/_c \} \cdot \hat{\lambda}_{BC} &= \{ \underline{r}_{G/c} \times m \underline{a} \} \cdot \hat{\lambda}_{BC} \\ &= \{ (l \hat{j} + h \hat{k}) \times m (\frac{F}{2m} \hat{j}) \} \cdot \hat{\lambda}_{BC} \\ &= \{ -F \frac{h}{2} \hat{i} \} \cdot \frac{\frac{b}{2} \hat{i} + l \hat{j}}{\sqrt{(\frac{b}{2})^2 + l^2}} \end{aligned}$$

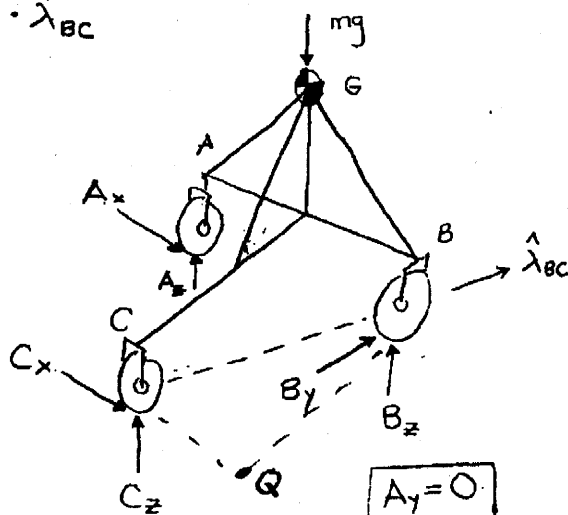
$$= -\frac{Fbh}{4} \cdot \frac{1}{\sqrt{(\frac{b}{2})^2 + l^2}}$$

$$\Rightarrow \{ \underline{\Sigma M}/_c = \dot{H}/_c \} \cdot \hat{\lambda}_{BC}$$

$$\frac{bl}{2} (A_z - mg) + \frac{bl}{2} A_z = -\frac{Fbh}{4}$$

$$bl A_z = \frac{mgbl}{2} - \frac{Fbh}{4}$$

$$\therefore \boxed{A_z = \frac{mg}{2} - \frac{Fh}{4l}}$$



• Now get A_x by taking $\underline{\Delta MB}/_a \cdot \hat{k}$

$$\underline{\Delta MB}/_a : \{ \underline{\Sigma M}/_a = \dot{H}/_a \} \cdot \hat{k}$$

The only force creating a moment about Q in the \hat{k} -direction is A_x !

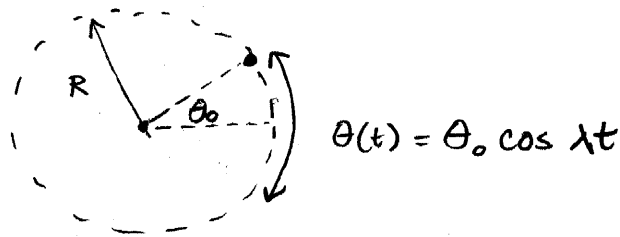
$$\begin{aligned} \Rightarrow \underline{\Sigma M}/_a \cdot \hat{k} &= \{ \underline{r}_{A/a} \times A_x \hat{i} \} \cdot \hat{k} \\ &= \{ (-b \hat{i} + l \hat{j}) \times A_x \hat{i} \} \cdot \hat{k} \\ &= \{ -A_x l \hat{k} \} \cdot \hat{k} = -A_x l \end{aligned}$$

$$\begin{aligned} \dot{H}/_a \cdot \hat{k} &= \{ \underline{r}_{G/a} \times m \underline{a} \} \cdot \hat{k} \\ &= \{ (-\frac{b}{2} \hat{i} + l \hat{j} + h \hat{k}) \times m (\frac{F}{2m} \hat{j}) \} \cdot \hat{k} \\ &= \{ \frac{F}{2} (-\frac{b}{2} \hat{k} - h \hat{i}) \} \cdot \hat{k} \\ &= -\frac{Fb}{4} \end{aligned}$$

$$\Rightarrow \{ \underline{\Sigma M}/_a = \dot{H}/_a \} \cdot \hat{k}$$

$$-A_x l = -\frac{Fb}{4} \Rightarrow \boxed{A_x = \frac{Fb}{4l}}$$

#13.13



The acceleration of a particle moving in circular motion w/ given $\theta(t)$ is

$$\begin{aligned} \underline{a}(t) &= -R\dot{\theta}^2 \hat{e}_r + R\ddot{\theta} \hat{e}_\theta \\ &= -R[-\lambda\theta_0 \sin \lambda t]^2 \hat{e}_r - R\lambda^2 \theta_0 \cos \lambda t \hat{e}_\theta \\ &= -R\lambda^2 [\theta_0^2 - \theta_0^2 \cos^2 \lambda t] \hat{e}_r - R\lambda^2 \theta_0 \cos \lambda t \hat{e}_\theta \\ \Rightarrow \underline{a}(\theta(t)) &= -R\lambda^2 (\theta_0^2 - \theta^2) \hat{e}_r - R\lambda^2 \theta \hat{e}_\theta \end{aligned}$$

where $\theta \in [\theta_0, \theta_0]$. Thus

$$\begin{aligned} \|\underline{a}\| &= (R^2 \lambda^4 [\theta_0^2 - \theta^2]^2 + R^2 \lambda^4 \theta^2)^{1/2} \\ &= (R^2 \lambda^4 \theta_0^4 - 2R^2 \lambda^4 \theta_0^2 \theta^2 + R^2 \lambda^4 \theta^4 + R^2 \lambda^4 \theta^2)^{1/2} \end{aligned}$$

From Calculus, $\|\underline{a}\|$ is extremized when either $\theta = \pm \theta_0$ or

$$\frac{d\|\underline{a}\|}{d\theta} \Big|_{\theta = \theta_E} = 0$$

$$= \frac{1}{2} \left[\quad \right]^{-1/2} (-4R^2 \lambda^4 \theta_0^2 \theta_E + 4R^2 \lambda^4 \theta_E^3 + 2R^2 \lambda^4 \theta_E)$$

Thus θ_E must satisfy

$$\theta_E [-4R^2 \lambda^4 \theta_0^2 + 2R^2 \lambda^4 + 4R^2 \lambda^4 \theta_E^2] = 0$$

$$\Rightarrow \theta_E = 0, \quad \pm \sqrt{\theta_0^2 - \frac{1}{2}}$$

These are local minima for $\theta_0^2 > \frac{1}{2}$ so we ignore them...

For $\theta_E = 0$ to be a ^{local} maximum it must satisfy

$$\left. \frac{d^2 \|\underline{a}\|}{d\theta^2} \right|_{\theta=0} < 0$$

This derivative is a little messy, but when we plug in $\theta = 0$ we get

$$\left. \frac{d^2 \|\underline{a}\|}{d\theta^2} \right|_{\theta=0} = \frac{(1 - 2\theta_0^2)R\lambda^2}{\theta_0^2}$$

$$\Rightarrow \boxed{\theta_0^2 > \frac{1}{2}}$$

~~UNNECESSARY~~

Finally, for $\theta = 0$ to be a global maximum we must compare $\|\underline{a}(0)\|$ & $\|\underline{a}(\pm\theta_0)\|$.

$$\|\underline{a}(0)\| = \theta_0^2 R \lambda^2$$

$$\|\underline{a}(\pm\theta_0)\| = |\theta_0| R \lambda$$

Thus $\|\underline{a}(0)\| > \|\underline{a}(\pm\theta_0)\|$ when $|\theta_0| > 1$.

Therefore $\theta = 0$ maximizes $\|\underline{a}\|$ when $|\theta_0| > 1$.